

# STRUCTURAL CALCULATIONS

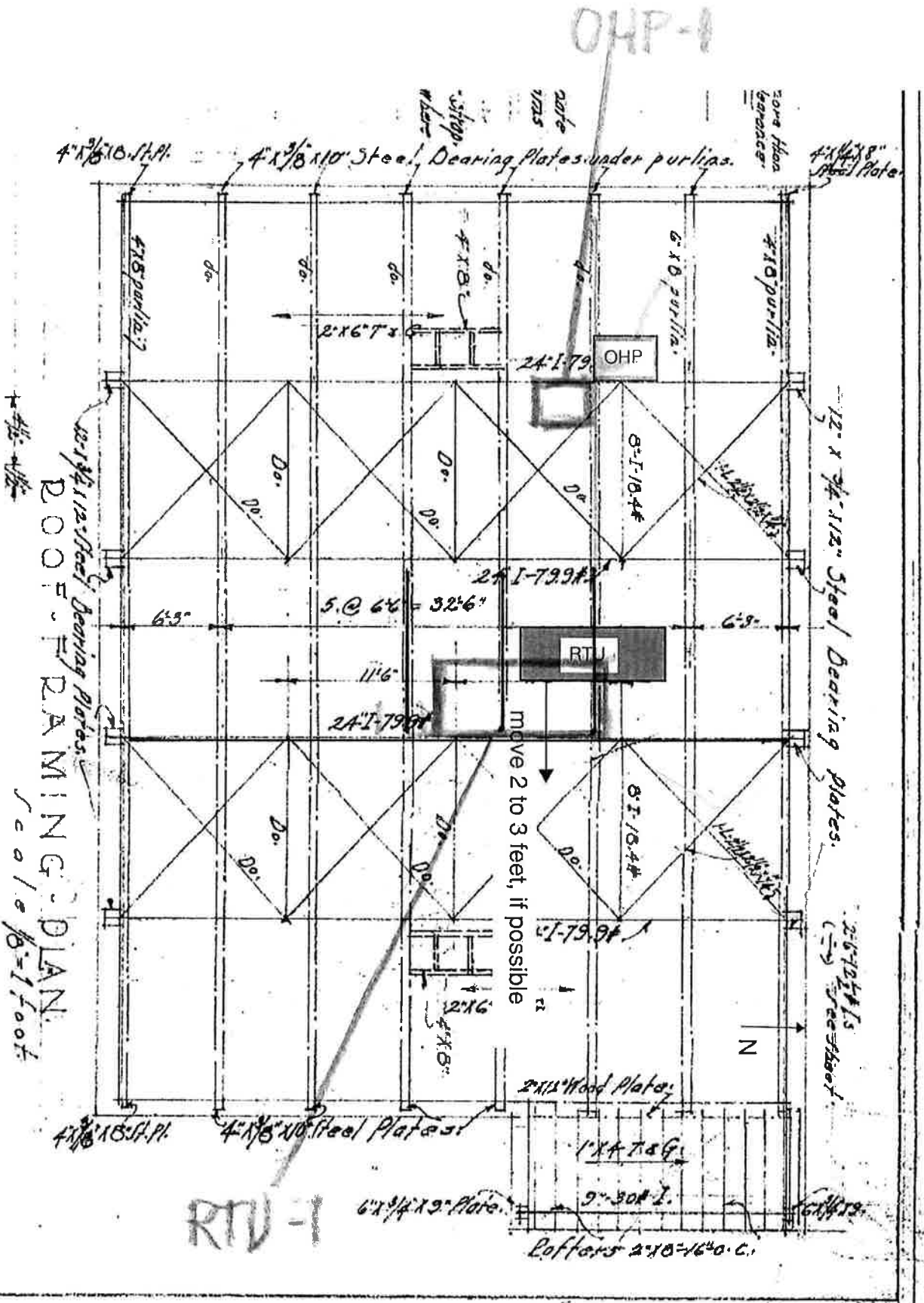
**PROJECT:** Ainsworth Elementary School  
Portland, Oregon  
New Rooftop Units Calculations  
**PROJECT No.:** A18142  
**DATE:** September 28, 2018

## PERMIT SUBMITTAL



**Contents:**

Structural Calculations	1 – 21
References	R1 – R6



ROOF FRAMING PLAN

See 0108-1-foot

RTU-1

OHP-1

12' x 3/4 x 12' Steel Bearing Plates.

2x 12 Wood Plates  
1' x 4' x 6' G.  
6' x 3/4 x 9' Plate  
9' x 30# I.  
Potters 2 x 10-16' O.C.

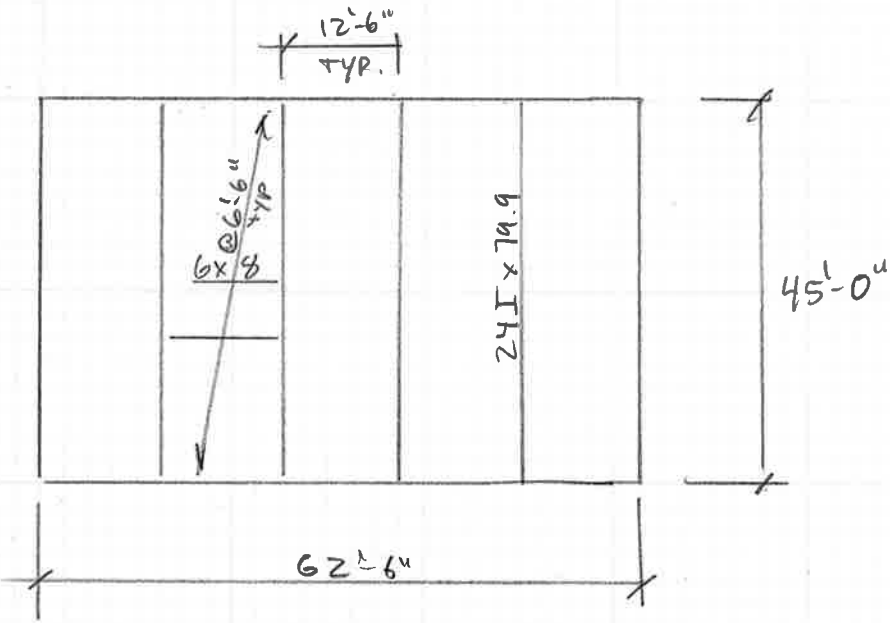
<b>ROOF</b>	<b>Description</b>	
Roof LL	standard min.	20 psf
Roof SL	(not incl. drift)	25 psf
Roof DL		
Roofing:	composition	3.0 psf
Plywood:	2x6 flat	1.5 psf
Joists:	6x8 @ 6.5'	2.0 psf
Insulation:	Foam	2.0 psf
Beams/Girders:	24I x 80 @ 12'	6.7 psf
Columns:	na	0.0 psf
Ceiling:	n/a	0.0 psf
Fire Sprinkler:		2.0 psf
MEP:		1.5 psf
Other (specify):		0.0 psf
Misc:		1.0 psf
DL Joists		13.0 psf
DL Beams		20.0 psf
DL Columns		20 psf

**Mechanical Units**

Concrete Pad	0 psf
RTU 1	1700 lb
OHP 1	300 lb
	0 lb

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# ROOF CHECKS FOR NEW UNITS



DL = 20 psf.  
SL = 25 psf.

RTU = 1700 lb  
OHP = 294 lb

## CHECK 24I (AISC Eq. 1 1928)

W/O NEW UNITS

$$W_D = 20 \text{ psf} \times 12.5' = 250 \text{ plf.}$$

$$W_S = 25 \times 12.5' = 313 \text{ plf.}$$

$$563 \text{ plf.}$$

SECTION PROP:

$$A = 23.33 \text{ m}^2$$

$$I_x = 2087.2 \text{ m}^4$$

$$S_x = 173.93 \text{ m}^3$$

$$b_f = 7.0''$$

$$t_f = 0.6''$$

$$t_w = 0.5''$$

$$M = 0.563 \text{ klf} \times 45' \times 12'' = 1710 \text{ k-in}$$

$$M/S = 1710 / 173.93 = 9.83 \text{ ksi}$$

LOW STRESS

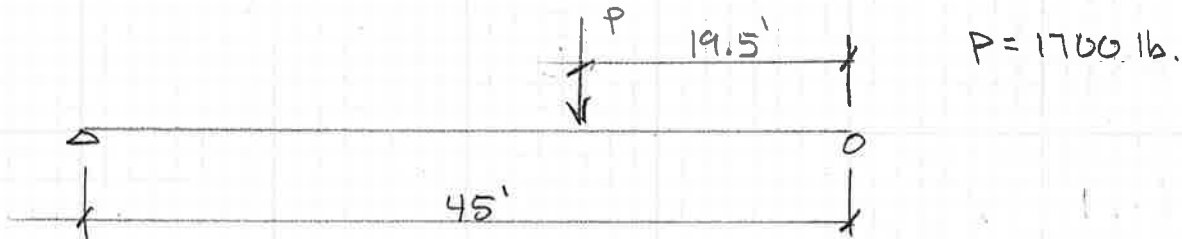
1924

$$F_u = 55 \text{ ksi}$$

$$F_y = \frac{1}{2} F_u \approx 25 \text{ ksi}$$

ADD RTU-1 LOADS TO 24I

RESOLVE TO A SINGLE POINT LOAD:



$$M = \frac{1.7k \times 19.5 \times 25.5' \times 12''}{45'} = 19 k''$$

$$M/S = 19 / 173.93 = 0.11 ksi$$

TOTAL STRESS  $\approx$  10 ksi

$$M_{TL} = M_a = (19 k'' + 1710 k'') / 12 = 144 k'$$

$$M_n / S_b = 241 k' \gg M_a \quad @ F_y = 25 ksi$$

W24 x 76

ASSUMING  $L_u = 45' / 4 \text{ BAY} = 11.25'$  (HORIZ. BRACE BAYS)

$\therefore$  EXISTING 24I OK

**Beam Calculator based on AISC Manual 13th edition**

Try :	<b>W24X76</b>	Member
unbraced length	<b>11.25</b>	ft.

**ASD Design**

$M_n / \Omega_b =$	<b>241.89</b>	k-ft.
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**Limiting Width Thickness Ratios for Compression Elements**  
(See section 16.1-16 AISC TABLE B4.1)

Case			$\lambda_p$	$\lambda_r$		
1	$b/t_f$	6.61	12.9	34.06	Compact	flanges
9	$h/t_w$	49.00	128.1	194.1	Compact	webs

**Noncompact or Slender Flange (See section F3. AISC 16.1-47)**

$M_n / \Omega_b =$	NA	k-ft.
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**Member Properties**

$F_y$	<b>25</b>	ksi
$E$	<b>29000</b>	ksi
$A$	<b>22.4</b>	in. <sup>2</sup>
$Z_x$	<b>200</b>	in. <sup>3</sup>
$S_x$	<b>176</b>	in. <sup>3</sup>
$S_y$	<b>18.4</b>	in. <sup>3</sup>
$I_x$	<b>2100</b>	in. <sup>4</sup>
$I_y$	<b>82.5</b>	in. <sup>4</sup>
$L_p$	<b>9.59</b>	ft.
$L_r$	<b>30.49</b>	ft.
$F_{cr}$	<b>92.42</b>	ksi
$r_y$	<b>1.92</b>	in.
$b_f$	<b>8.99</b>	in.
$t_w$	<b>0.44</b>	in.
$t_f$	<b>0.68</b>	in.
$J$	<b>2.68</b>	in. <sup>4</sup>
$C_w$	<b>11100</b>	in. <sup>6</sup>
$r_{at}$	<b>2.33</b>	in.
$h_o$	<b>23.2</b>	in.
$h/t_w$	<b>49.0</b>	in.
$k_c$	<b>0.6</b>	
$c$	<b>1.0</b>	in.

in.

# Historical Listing of Selected Structural Steels

## CSA Standards

Designation	Date Published	Yield Strength		Tensile Strength ( $F_u$ )	
		ksi	MPa	ksi	MPa
A16	1924	$\frac{1}{2} F_u$	$\frac{1}{2} F_u$	55 - 65	380 - 450
S39	1935	30	210	55 - 65	380 - 450
S40	1935	33	230	60 - 72	410 - 500
G40.4	1950	33	230	60 - 72	410 - 500
G40.5	1950	33	230	60 - 72	410 - 500
G40.6	1950	45 <sup>1</sup>	310	80 - 95	550 - 650
G40.8	1960	40 <sup>3</sup>	280	65 - 85	450 - 590
G40.12	1964 *	44 <sup>2</sup>	300	65	450
G40.21	1973 **	Replaced all previous Standards, see CISC Handbook			

\* Introduced in May 1962 by the Algoma Steel Corporation as "Algoma 44"

\*\* In May 1997, grade 350W became the only grade for W and HP shapes produced by Algoma Steel Inc.

<sup>1</sup> Silicon steel

<sup>2</sup> Yield reduces when thickness exceeds 1½ inches (40 mm).

<sup>3</sup> Yield reduces when thickness exceeds ¾ inches (16 mm).

## Rivet Steel

Designation	Date Published	Yield Strength		Tensile Strength ( $F_u$ )	
		ksi	MPa	ksi	MPa
G40.2	1950	28	190	52 - 62	360 - 430

## ASTM Specifications

Designation	Date Published	Yield Strength		Tensile Strength ( $F_u$ )	
		ksi	MPa	ksi	MPa
A7 (bridges)	1914*	$\frac{1}{2} F_u$	$\frac{1}{2} F_u$	55 - 65	380 - 450
A9 (buildings)	1924	$\frac{1}{2} F_u \geq 30$	$\frac{1}{2} F_u \geq 210$	55 - 65	380 - 450
	1934	$\frac{1}{2} F_u \geq 33$	$\frac{1}{2} F_u \geq 230$	60 - 72	410 - 500
A373	1954	32	220	58 - 75	400 - 520
A242	1955	50 <sup>1</sup>	350	70 <sup>1</sup>	480
A36	1960	36	250	60 - 80	410 - 550
A440	1959	50 <sup>1</sup>	350	70 <sup>1</sup>	480
A441	1960	50 <sup>1</sup>	350	70 <sup>1</sup>	480
A572 grade 50	1966	50	345	65	450
A588	1968	50 <sup>1</sup>	345	70 <sup>1</sup>	485
A992	1998	50 min. to 65 max.	345 min. to 450 max.	65	450

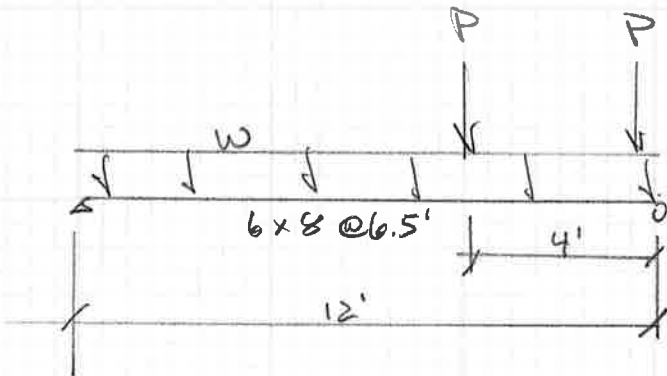
<sup>1</sup> Reduces with increasing thickness

\* Between 1900 and 1909, medium steel in A7 and A9 had a tensile strength 5 ksi higher than that adopted in 1914.

Reference: Handbook of Steel Construction, 8th Edition, CISC, 2004.

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CHECK 6x8 PURLIN w/ 1700 lb RTU-1



• 6x8 DFL NO. 2

$$A = 5.5 \times 7.5 = 41.3 \text{ in}^2$$

$$S = 5.5 \times 7.5^2 / 6 = 51.7 \text{ in}^3$$

$$F_b = 875 \text{ psi}$$

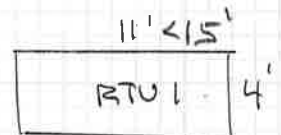
$$F_v = 170 \text{ psi}$$

$$W_D = 20 \text{ psf} \times 6.5' = 130 \text{ plf}$$

$$W_S = 25 \text{ psf} \times 6.5' = 163 \text{ plf}$$

$$\Sigma_{TL} = 293 \text{ plf}$$

$$P = (1700 \times \frac{1}{2}) / 2 = 425 \text{ lb}$$



NEGLECT DRIFT.

Total D+S+RTU

$$M_{D+S} = 293 \times 12^2 / 8 \times 12" / 1 = 63288 \text{ lb.in.}$$

$$M_{RTU} = 425 \times 4' \times 8' / 12' \times 12" / 1 = 13600 \text{ lb.in.}$$

$$M_{TL} = 76888 \text{ lb.in.}$$

$$V_{TL} = 293 \text{ plf} \times 6' + 425 \text{ lb} \times 2 = 2608 \text{ lb}$$

$$C_D = 1.15$$

$$F'_b = 875 \times 1.15 \times 1.29 = 1298 \text{ psi}$$

$$C_F = 1.29 \text{ (} F_b \text{ only)}$$

$$F'_v = 170 \times 1.15 = 196 \text{ psi}$$

$$F_b = M / S = 76888 / 51.7 = 1487 \text{ psi} > F'_b$$

$$F_v = 3 \times 2608 / (2 \times 41.3) = 95 \text{ psi} < F'_v$$



FOR D + RTU

$C_D = 0.9$

$M_D = 130 \text{ pF} \times 12^2/8 \times 12'' = 28080 \text{ lb.in.}$

$M_{RTU} = \frac{13600 \text{ lb.in.}}{41680 \text{ lb.in.}}$

$M_{th}$

$V_{th} = 130 \times 6' + 425 \text{ lb} \times 2 = 1630 \text{ lb.}$

$F_b = M/S = 806 \text{ psi} < F'_b = 875 \times .9 \times 1.29 = 1016 \text{ psi}$

$F_v = 3 \times 1630 / (2 \times 41.3) = 59.2 \text{ psi} < F'_v = 170 \times .9 = 153 \text{ psi}$

∴ OK FOR D + UNIT

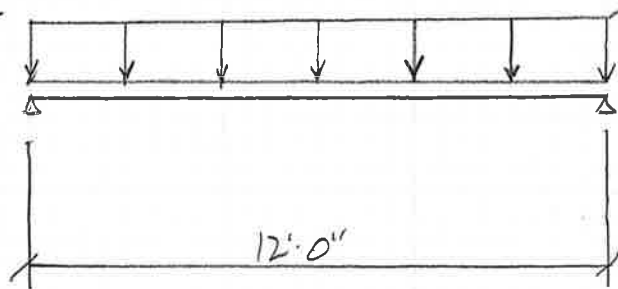
SUMMARY

D + S + RTU	DFL No. 2	FLEXURE <u>NG</u> SHEAR OK.
D + RTU	DFL No. 2	FLEXURE OK. SHEAR OK.

WOULD BE OK w/ DFL No. 1  
NEED TO CONFIRM GRADE

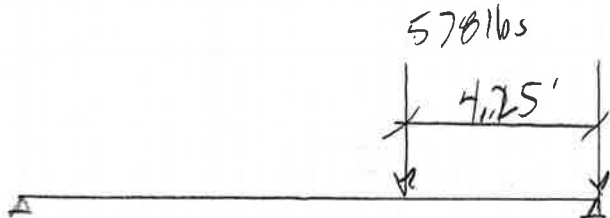
# MORE PRECISE CHECK ON 6x8 PURLINS

## BASE LOAD

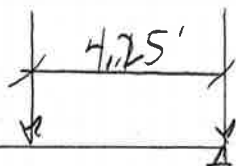


$$6.5' \times (13 + 25) = 85 + 163 = 248 \text{ plf}$$

## RTU DEAD LOAD



578 lbs



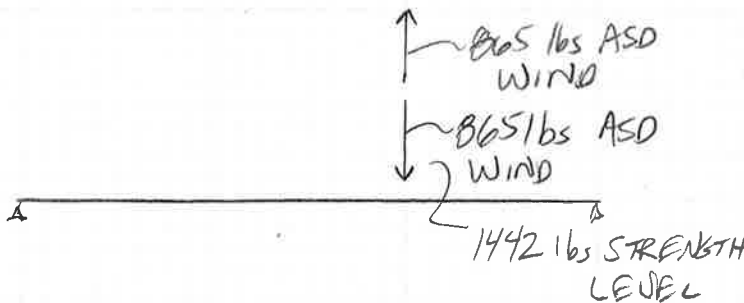
$$\left( \frac{1700 \text{ lbs}}{2} / 11'0" \right) = 77 \text{ plf}$$

$$\times 6.5' = 503 \text{ lbs}$$

$$\times 1.15 = 578 \text{ lbs}$$

INCREASE TO ACCOUNT FOR CURBS AND ANY UNBALANCED ASPECT TO LOAD.

## RTU WIND LOAD



SEE ATTACHED ENERCALC PRINTOUT

O.T.

$$\frac{73103 \text{ @ } 11\text{-lbs}}{50 \text{ m}}$$

$$= 1463 \text{ lbs} / 11'$$

$$133 \text{ plf} \times 6.5' =$$

$$865 \text{ lbs}$$

ASSUMING DF-L#2, THE PROPOSED INSTALLATION IS 34% OVERSTRESSED

ASSUMING DF-L#1, THE PROPOSED INSTALLATION IS ACCEPTABLE WITH SR = 0.866



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AINSWORTH ELEMENTARY  
NEW ROOFTOP UNITS

By: DEL Date: 9/24/13

Project No.: A18142

Sheet: 9 of 21

**Wood Beam**

File = F:\2018\A18142.00 - Ainsworth School RTU and Foundation Repair\structural\Ainsworth RTUs.ec6  
ENERCALC, INC. 1983-2018, Build:10.18.1.31, Ver:10.18.1.31

Lic. #: KW-06009892

Licensee : AAI Engineering

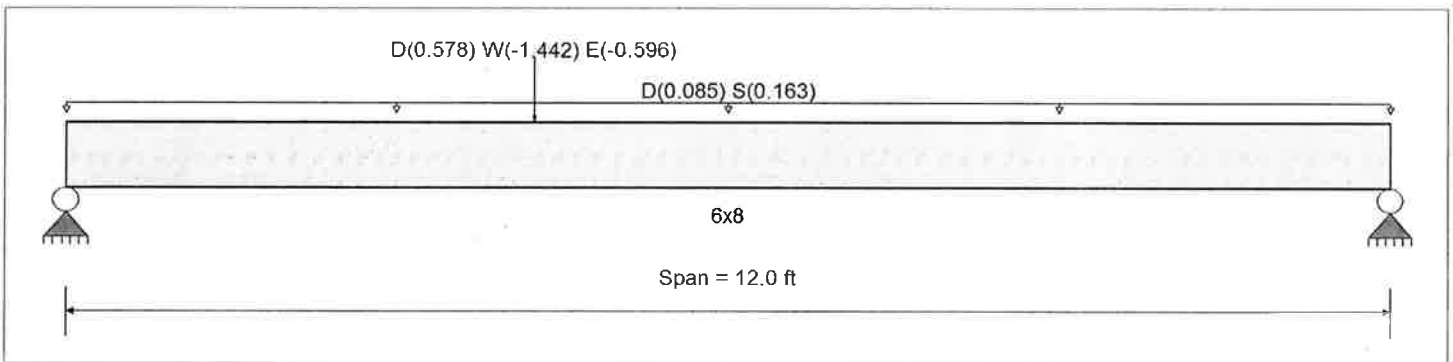
Description : Ainsworth Elementary School - 6x8 Purlins with RTU's - Proposed Load

**CODE REFERENCES**

Calculations per NDS 2015, IBC 2015, CBC 2016, ASCE 7-10  
Load Combination Set : ASCE 7-10

**Material Properties**

Analysis Method : Allowable Stress Design	Fb +	1,350.0 psi	E : Modulus of Elasticity
Load Combination ASCE 7-10	Fb -	1,350.0 psi	Ebend- xx
	Fc - Prll	925.0 psi	Eminbend - xx
Wood Species : Douglas Fir - Larch	Fc - Perp	625.0 psi	
Wood Grade : No. 1	Fv	170.0 psi	
	Ft	675.0 psi	Density
Beam Bracing : Beam is Fully Braced against lateral-torsional buckling			31.20 pcf



**Applied Loads**

Service loads entered. Load Factors will be applied for calculations.

Uniform Load : D = 0.0850, S = 0.1630, Tributary Width = 1.0 ft

Point Load : D = 0.5780, W = -1.442, E = -0.5960 k @ 4.250 ft

**DESIGN SUMMARY**

**Design OK**

Maximum Bending Stress Ratio	=	<b>0.866</b>	1	Maximum Shear Stress Ratio	=	<b>0.318</b>	: 1
Section used for this span		<b>6x8</b>		Section used for this span		<b>6x8</b>	
fb : Actual	=	1,344.40	psi	fv : Actual	=	62.15	psi
FB : Allowable	=	1,552.50	psi	Fv : Allowable	=	195.50	psi
Load Combination		+D+S+H		Load Combination		+D+S+H	
Location of maximum on span	=	5.168	ft	Location of maximum on span	=	0.000	ft
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	=	Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.247	in	Ratio =		582	>=360
Max Upward Transient Deflection		-0.109	in	Ratio =		1317	>=360
Max Downward Total Deflection		0.480	in	Ratio =		300	>=180
Max Upward Total Deflection		0.000	in	Ratio =		0	<180

**Overall Maximum Deflections**

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+S	1	0.4798	5.912		0.0000	0.000

**Vertical Reactions**

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Overall MAXimum	1.861	1.693
Overall MINimum	1.198	1.218
+D+H	0.883	0.715
+D+L+H	0.883	0.715
+D+Lr+H	0.883	0.715

10/21

**Wood Beam**

File = F:\2018\A18142.00 - Ainsworth School RTU and Foundation Repair\structural\Ainsworth RTUs.ec6  
 ENERCALC, INC. 1983-2018, Build:10.18.1.31, Ver:10.18.1.31

Lic. #: KW-06009892

Licensee: AAI Engineering

Description: Ainsworth Elementary School - 6x8 Purlins with RTU's - Proposed Load

**Vertical Reactions**

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
+D+S+H	1.861	1.693
+D+0.750Lr+0.750L+H	0.883	0.715
+D+0.750L+0.750S+H	1.617	1.448
+D+0.60W+H	0.325	0.408
+D+0.70E+H	0.614	0.567
+D+0.750Lr+0.750L+0.450W+H	0.464	0.485
+D+0.750L+0.750S+0.450W+H	1.198	1.218
+D+0.750L+0.750S+0.5250E+H	1.415	1.337
+0.60D+0.60W+0.60H	-0.029	0.122
+0.60D+0.70E+0.60H	0.261	0.281
D Only	0.883	0.715
Lr Only		
L Only		
S Only	0.978	0.978
W Only	-0.931	-0.511
E Only	-0.385	-0.211
H Only		
+D+H	0.883	0.715
+D+L+H	0.883	0.715
+D+Lr+H	0.883	0.715
+D+S+H	1.861	1.693
+D+0.750Lr+0.750L+H	0.883	0.715
+D+0.750L+0.750S+H	1.617	1.448
+D+0.60W+H	0.325	0.408
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11/21

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Load Combination Set : ASCE 7-10

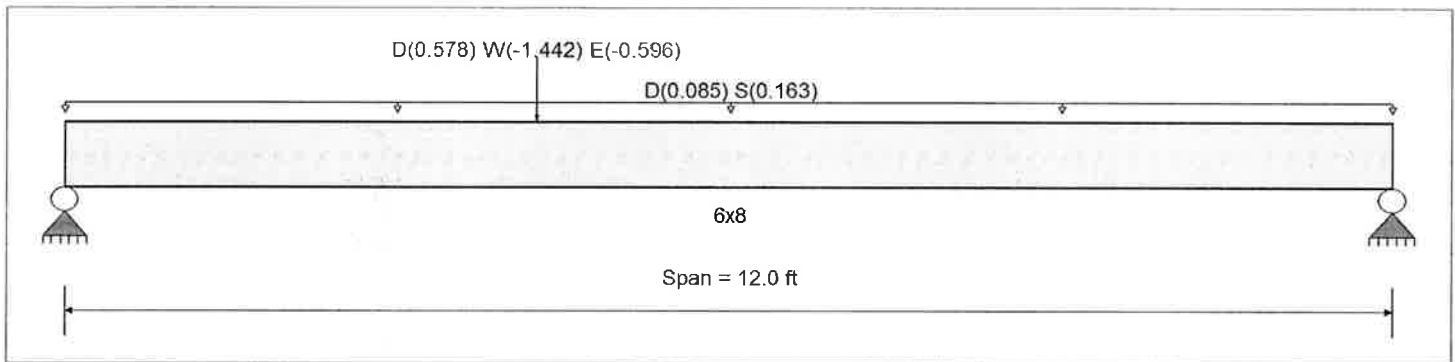
**Material Properties**

Analysis Method : Allowable Stress Design  
 Load Combination ASCE 7-10

Fb +	875 psi	E : Modulus of Elasticity	
Fb -	875 psi	Ebend- xx	1300 ksi
Fc - Prll	600 psi	Eminbend - xx	470 ksi
Fc - Perp	625 psi		
Fv	170 psi		
Ft	425 psi	Density	31.2pcf

Wood Species : Douglas Fir - Larch  
 Wood Grade : No.2

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling



**Applied Loads**

Service loads entered. Load Factors will be applied for calculations.

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Point Load : D = 0.5780, W = -1.442, E = -0.5960 k @ 4.250 ft

**DESIGN SUMMARY**

**Design N.G.**

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fb : Actual	=	1,344.40	psi	f <sub>v</sub> : Actual	=	62.15	psi
FB : Allowable	=	1,006.25	psi	F <sub>v</sub> : Allowable	=	195.50	psi
Load Combination		+D+S+H		Load Combination		+D+S+H	
Location of maximum on span	=	5.168	ft	Location of maximum on span	=	0.000	ft
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	=	Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.304	in	Ratio =		473	>=360
Max Upward Transient Deflection		-0.135	in	Ratio =		1070	>=360
Max Downward Total Deflection		0.591	in	Ratio =		243	>=180
Max Upward Total Deflection		0.000	in	Ratio =		0	<180

**Overall Maximum Deflections**

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+S	1	0.5906	5.912		0.0000	0.000

**Vertical Reactions**

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Overall MAXimum	1.861	1.693
Overall MINimum	1.198	1.218
+D+H	0.883	0.715
+D+L+H	0.883	0.715
+D+Lr+H	0.883	0.715

12/21

**Wood Beam**

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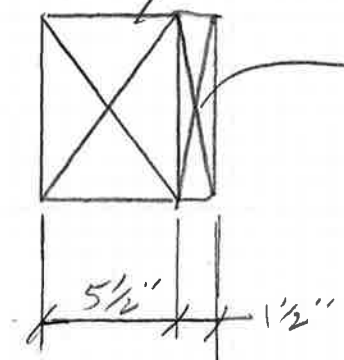
Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
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+D+0.750Lr+0.750L+H	0.883	0.715
+D+0.750L+0.750S+H	1.617	1.448
+D+0.60W+H	0.325	0.408
+D+0.70E+H	0.614	0.567
+D+0.750Lr+0.750L+0.450W+H	0.464	0.485
+D+0.750L+0.750S+0.450W+H	1.198	1.218
+D+0.750L+0.750S+0.5250E+H	1.415	1.337
+0.60D+0.60W+0.60H	-0.029	0.122
+0.60D+0.70E+0.60H	0.261	0.281
D Only	0.883	0.715
Lr Only		
L Only		
S Only	0.978	0.978
W Only	-0.931	-0.511
E Only	-0.385	-0.211
H Only		
+D+H	0.883	0.715
+D+L+H	0.883	0.715
+D+Lr+H	0.883	0.715
+D+S+H	1.861	1.693
+D+0.750Lr+0.750L+H	0.883	0.715
+D+0.750L+0.750S+H	1.617	1.448
+D+0.60W+H	0.325	0.408
+D+0.70E+H	0.614	0.567
+D+0.750Lr+0.750L+0.450W+H	0.464	0.485
+D+0.750L+0.750S+0.450W+H	1.198	1.218

13/21

REINFORCE OF 6x8 → ADD A 2x8 TO SIDE OF 6x8



6x8 DF-L #2  
 MOMENT CAPACITY = 4324 ft-lbs  
 $(1006.25 \text{ psi} \times \frac{5.5(7.5)(1)}{6} (\frac{1}{12}))$

2x8 DF-L #1  
 MOMENT CAPACITY = 1511 ft-lbs  
5835 ft-lbs

APPLIED MOMENT FROM ENERCALC  
 5.777 k-ft

SR = 0.99  
 DL + SL w/ MECH. UNIT

MOMENT WITH WIND —  $M_{max} = 6.78 \text{ k-ft}$   
 $M_{cap} = 5835 \times \frac{1.6}{1.15} =$   
 $8118 \text{ k-ft}$   
 SR = 83.5%

CONNECT 2 JOISTS TOGETHER SO THEY BEHAVE AS ONE

TOTAL SHEAR = 1.71 kips D+S →  $\times \frac{1.5}{7} = 366 \text{ lbs}$   
 1.91 kips D+0.75S+0.45W = 410 lbs

USE SDS SCREWS:  $\frac{1}{4}'' \phi \times 3\frac{1}{2}''$  SDS SCREWS  
 CAPACITY = 340 lbs  $\times 1.15 = 391 \text{ lbs}$   
 TRY (4) SCREWS EA. END.  
 1564 lbs OK EASILY  
 SR = 0.234

AAI ENGINEERING DESIGN AID  
WOOD MEMBER CAPACITIES

2X TO 4X DIMENSIONAL LUMBER

MODIFICATION FACTORS

DF-L #1	
$F_b$	1000 psi
$F_v$	180 psi
$F_b'$	1150 psi
$F_v'$	207 psi

$C_D$	$C_M$	$C_t$	$C_L$	$C_{fu}$	$C_i$	$C_r$
1.15	1.00	1.00	1.00	1.00	1.00	1.00
1.15	1.00	1.00	---	---	1.00	---

NOMINAL SIZE	b (in)	d (in)	AREA, A (in <sup>2</sup> )	$S_{xx}$ (in <sup>3</sup> )	$I_{xx}$ (in <sup>4</sup> )	$C_F$	$F_b'$ (psi)	M (ft-lbs)	V (lbs)	$I_{xx}$ (in <sup>4</sup> )
2 x 3	1.5	2.5	3.75	1.56	2.0	1.5	1725	225	518	1.95
2 x 4	1.5	3.5	5.25	3.06	5.4	1.5	1725	440	725	5.36
2 x 5	1.5	4.5	6.75	5.06	11.4	1.4	1610	679	932	11.4
2 x 6	1.5	5.5	8.25	7.56	20.8	1.3	1495	942	1,139	20.8
2 x 8	1.5	7.25	10.88	13.14	47.6	1.2	1380	1,511	1,501	47.6
2 x 10	1.5	9.25	13.88	21.39	98.9	1.1	1265	2,255	1,915	98.9
2 x 12	1.5	11.25	16.88	31.64	178.0	1	1150	3,032	2,329	178.0
2 x 14	1.5	13.25	19.88	43.89	290.8	0.9	1035	3,786	2,743	290.8
3 x 4	2.5	3.5	8.75	5.10	8.9	1.5	1725	734	1,208	8.9
3 x 5	2.5	4.5	11.25	8.44	19.0	1.4	1610	1,132	1,553	19.0
3 x 6	2.5	5.5	13.75	12.60	34.7	1.3	1495	1,570	1,898	34.7
3 x 8	2.5	7.25	18.13	21.90	79.4	1.2	1380	2,519	2,501	79.4
3 x 10	2.5	9.25	23.13	35.65	164.9	1.1	1265	3,758	3,191	164.9
3 x 12	2.5	11.25	28.13	52.73	296.6	1	1150	5,054	3,881	296.6
3 x 14	2.5	13.25	33.13	73.15	484.6	0.9	1035	6,309	4,571	484.6
3 x 16	2.5	15.25	38.13	96.90	738.9	0.9	1035	8,358	5,261	738.9
4 x 4	3.5	3.5	12.25	7.15	12.5	1.5	1725	1,027	1,691	12.5
4 x 5	3.5	4.5	15.75	11.81	26.6	1.4	1610	1,585	2,174	26.6
4 x 6	3.5	5.5	19.25	17.65	48.5	1.3	1495	2,198	2,657	48.5
4 x 8	3.5	7.25	25.38	30.66	111.1	1.3	1495	3,820	3,502	111.1
4 x 10	3.5	9.25	32.38	49.91	230.8	1.2	1380	5,740	4,468	230.8
4 x 12	3.5	11.25	39.38	73.83	415.3	1.1	1265	7,783	5,434	415.3
4 x 14	3.5	13.25	46.38	102.41	678.5	1.0	1150	9,814	6,400	678.5
4 x 16	3.5	15.25	53.38	135.66	1034.4	1.0	1150	13,001	7,366	1034.4
(2) 2 x 4	---	---	10.50	6.13	10.7	---	1725	880	1,449	10.7
(2) 2 x 6	---	---	16.5	15.13	41.6	---	1495	1,884	2,277	41.6
(2) 2 x 8	---	---	21.75	26.28	95.3	---	1380	3,022	3,002	95.3
(2) 2 x 10	---	---	27.75	42.78	197.9	---	1265	4,510	3,830	197.9
(2) 2 x 12	---	---	33.75	63.28	356.0	---	1150	6,064	4,658	356.0
(3) 2 x 4	---	---	15.75	9.19	16.1	---	1725	1,321	2,174	16.1
(3) 2 x 6	---	---	24.75	22.69	62.4	---	1495	2,826	3,416	62.4
(3) 2 x 8	---	---	32.63	39.42	142.9	---	1380	4,534	4,502	142.9
(3) 2 x 10	---	---	41.63	64.17	296.8	---	1265	6,765	5,744	296.8
(3) 2 x 12	---	---	50.63	94.92	533.9	---	1150	9,097	6,986	533.9

15/21



**Project:** AINSWORTH ELEMENTARY RTU'S  
**Location:** RTU 1 - GYMNASIUM ROOF  
**Subject:** Roof Top Unit Anchorage

**Unit Information:**

Weight 1700 lbs  
 New Weight 1955 lbs (weight increased by 15% to account for Curb and Misc. weights)  
 Dimensions: (inches)  
 width 50 in length 132 in Height 52 in  
 Curb Height 14 in

**Lateral Loads:**
**Wind Loads on other Structures and Building Appurtenances ASCE 7-10 Chapter 29**
**Input Parameters**

V 130 Wind Speed (Ultimate), MPH  
 K<sub>d</sub> 0.85 Wind directionality factor  
 K<sub>zt</sub> 1 Topographic factor  
 Exp. Cat. B Exposure Category  
 h 25 height above ground (ft)  
 K<sub>h</sub> 0.66 Velocity pressure exposure coefficient, Table 29.3.1  
 q<sub>h</sub> 24.27 Velocity pressure, Eq. 29.3-1, (PSF)  
 GCr 1.9  
 A<sub>f</sub> Long. 47.7 ft<sup>2</sup> A<sub>f</sub> short. 18.1 ft<sup>2</sup>  
 A<sub>f</sub> Long. w/curb 60.5 ft<sup>2</sup> A<sub>f</sub> short. w/curl 22.9 ft<sup>2</sup>

Lateral Wind Force (Unit Only):		Lateral Wind Force (Unit + Curb):	
F <sub>h</sub> Long.	2198 lb (ult)	2790 lb (ult)	q <sub>h</sub> (GCr)A <sub>f</sub> Eq. 29.5-2
F <sub>h</sub> Long.	1319 lb (ASD)	1674 lb (ASD)	
F <sub>h</sub> short.	833 lb (ult)	1057 lb (ult)	q <sub>h</sub> (GCr)A <sub>f</sub> Eq. 29.5-2
F <sub>h</sub> short.	500 lb (ASD)	634 lb (ASD)	

**Vertical Uplift Force**

G<sub>cr</sub> 1.5  
 A<sub>r</sub> 45.8 ft<sup>2</sup>  
 q<sub>h</sub> 24.27 PSF

F <sub>v</sub>	1669 lb (ult)	q <sub>h</sub> (GCr)A <sub>r</sub> Eq. 29.5-3
F <sub>v</sub>	1001 lb (ASD)	

**Seismic Anchorage Non-Structural Components ASCE 7-10 Chapter 13**
**Input Parameters**

S<sub>Ds</sub> 0.731 Design Spectral Acceleration  
 I<sub>p</sub> 1 Component Importance Factor  
 z 25 Component height  
 h 25 Total Structure Height

**Component Type**

R<sub>p</sub> 2.5 Component Response Modification Factor ASCE 7-10 Table 13.6-1  
 a<sub>p</sub> 2.5 Component Amplification Factor ASCE 7-10 Table 13.6-1

**Component Acceleration Factor**

F<sub>p</sub> 0.877 W<sub>p</sub> F<sub>pmax</sub> 1.17 W<sub>p</sub> F<sub>pmin</sub> 0.219 W<sub>p</sub>

Use F<sub>p</sub> 0.877 W<sub>p</sub> **Component Horizontal Acceleration**

F <sub>p</sub> Long.	1714.9 lbs (ult)	F <sub>p</sub> short	1714.9 lbs (ult)
F <sub>p</sub> Long.	1224.9 lbs (ASD)	F <sub>p</sub> short	1224.9 lbs (ASD)

**Component Vertical Acceleration**

F<sub>p,v</sub> 0.15 W<sub>p</sub> 0.2S<sub>Ds</sub>W<sub>p</sub> F<sub>p,v</sub> 0.10234 W<sub>p</sub> ASD

**Anchorage Design:**

Check Overturning:

Load Combinations: Seismic - (0.6 -Ev)D+0.7E (ASD)

Wind - 0.6D+0.6W (ASD)

**Load Parallel to Short Direction:**
**WIND AT TOP OF CURB**

Mot: 62750 lbs-in

Mresisting: 25500 lbs-in

**WIND AT BASE OF CURB**

Mot: 85795 lbs-in

Mresisting: 25500 lbs-in

Uplift:	745 lbs (ASD)	Uplift:	1206 lbs (ASD)
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Shear:	1319 lbs (ASD)	Shear:	1674 lbs (ASD)
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**SEISMIC AT TOP OF CURB**

Mot: 35033 lbs-in

Mresisting: 21151 lbs-in

**SEISMIC AT BASE OF CURB**

Mot: 52183 lbs-in

Mresisting: 21151 lbs-in

Uplift:	277.6587657 lbs (ASD)	Uplift:	620.64397 lbs (ASD)
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Shear:	1225 lbs (ASD)	Shear:	1225 lbs (ASD)
--------	----------------	--------	----------------

**Load Parallel to Long Direction :**
**WIND AT TOP OF CURB**

Mot: 80366 lbs-in

Mresisting: 67320 lbs-in

**WIND AT BASE OF CURB**

Mot: 89095 lbs-in

Mresisting: 67320 lbs-in

Uplift:	99 lbs (ASD)	Uplift:	165 lbs (ASD)
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Shear:	500 lbs (ASD)	Shear:	634 lbs (ASD)
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**SEISMIC AT TOP OF CURB**

Mot: 35033 lbs-in

Mresisting: 55837 lbs-in

**SEISMIC AT BASE OF CURB**

Mot: 52183 lbs-in

Mresisting: 55837 lbs-in

Uplift:	0 lbs (ASD)	Uplift:	0 lbs (ASD)
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Shear:	1225 lbs (ASD)	Shear:	1225 lbs (ASD)
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**Check Global Uplift due to wind:**

Uplift Force: 1001 lbs

Weight of Unit resisiting: 1020 lbs

Net uplift:	0 lbs (ASD)
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**Project:** AINSWORTH ELEMENTARY RTU'S  
**Location:** OHA 1 - GYMNASIUM ROOF  
**Subject:** Roof Top Unit Anchorage

**Unit Information:**

Weight 300 lbs  
 New Weight 345 lbs (weight increased by 15% to account for Curb and Misc. weights)  
 Dimensions: (inches)  
 width 34.25 in length 37.25 in Height 46 in  
 Curb Height 14 in

**Lateral Loads:**
**Wind Loads on other Structures and Building Appurtenances ASCE 7-10 Chapter 29**
**Input Parameters**

V 130 Wind Speed (Ultimate), MPH  
 K<sub>d</sub> 0.85 Wind directionality factor  
 K<sub>zt</sub> 1 Topographic factor  
 Exp. Cat. B Exposure Category  
 h 25 height above ground (ft)  
 K<sub>h</sub> 0.66 Velocity pressure exposure coefficient, Table 29.3.1  
 q<sub>h</sub> 24.27 Velocity pressure, Eq. 29.3-1, (PSF)  
 GCr 1.9  
 Af Long. 11.9 ft<sup>2</sup> Af short. 10.9 ft<sup>2</sup>  
 Af Long. w/curb 15.5 ft<sup>2</sup> Af short. w/curl 14.3 ft<sup>2</sup>

Lateral Wind Force (Unit Only):		Lateral Wind Force (Unit + Curb):	
F <sub>h</sub> Long.	549 lb (ult)	716 lb (ult)	q <sub>h</sub> (GCr)Af Eq. 29.5-2
F <sub>h</sub> Long.	329 lb (ASD)	429 lb (ASD)	
F <sub>h</sub> short.	505 lb (ult)	658 lb (ult)	q <sub>h</sub> (GCr)Af Eq. 29.5-2
F <sub>h</sub> short.	303 lb (ASD)	395 lb (ASD)	

**Vertical Uplift Force**

Gcr 1.5  
 Ar 8.9 ft<sup>2</sup>  
 q<sub>h</sub> 24.27 PSF

F <sub>v</sub>	323 lb (ult)	q <sub>h</sub> (GCr)Ar Eq. 29.5-3
F <sub>v</sub>	194 lb (ASD)	

**Seismic Anchorage Non-Structural Components ASCE 7-10 Chapter 13**
**Input Parameters**

S<sub>DS</sub> 0.731 Design Spectral Acceleration  
 I<sub>p</sub> 1 Component Importance Factor  
 z 25 Component height  
 h 25 Total Structure Height

**Component Type**

R<sub>p</sub> 2.5 Component Response Modification Factor ASCE 7-10 Table 13.6-1  
 a<sub>p</sub> 1 Component Amplification Factor ASCE 7-10 Table 13.6-1

**Component Acceleration Factor**

F<sub>p</sub> 0.351 W<sub>p</sub> F<sub>pmax</sub> 1.17 W<sub>p</sub> F<sub>pmin</sub> 0.219 W<sub>p</sub>  
 Use F<sub>p</sub> 0.351 W<sub>p</sub> **Component Horizontal Acceleration**

F <sub>p</sub> Long.	121.1 lbs (ult)	F <sub>p</sub> short	121.1 lbs (ult)
F <sub>p</sub> Long.	86.5 lbs (ASD)	F <sub>p</sub> short	86.5 lbs (ASD)

**Component Vertical Acceration**

F<sub>p,v</sub> 0.15 W<sub>p</sub> 0.2S<sub>DS</sub>W<sub>p</sub> F<sub>p,v</sub> 0.10234 W<sub>p</sub> ASD

**Anchorage Design:**

Check Overturning:

Load Combinations: Seismic - (0.6 -Ev)D+0.7E (ASD)  
Wind - 0.6D+0.6W (ASD)

**Load Parallel to Short Direction:**

**WIND AT TOP OF CURB**

Mot: 11644 lbs-in  
Mresisting: 3083 lbs-in

**WIND AT BASE OF CURB**

Mot: 17486 lbs-in  
Mresisting: 3083 lbs-in

Uplift:	250 lbs (ASD)	Uplift:	421 lbs (ASD)
Shear:	329 lbs (ASD)	Shear:	429 lbs (ASD)

**SEISMIC AT TOP OF CURB**

Mot: 2188 lbs-in  
Mresisting: 2557 lbs-in

**SEISMIC AT BASE OF CURB**

Mot: 3398 lbs-in  
Mresisting: 2557 lbs-in

Uplift:	0 lbs (ASD)	Uplift:	24.566985 lbs (ASD)
Shear:	86 lbs (ASD)	Shear:	86 lbs (ASD)

**Load Parallel to Long Direction :**

**WIND AT TOP OF CURB**

Mot: 11264 lbs-in  
Mresisting: 3353 lbs-in

**WIND AT BASE OF CURB**

Mot: 16635 lbs-in  
Mresisting: 3353 lbs-in

Uplift:	212 lbs (ASD)	Uplift:	357 lbs (ASD)
Shear:	303 lbs (ASD)	Shear:	395 lbs (ASD)

**SEISMIC AT TOP OF CURB**

Mot: 2188 lbs-in  
Mresisting: 2781 lbs-in

**SEISMIC AT BASE OF CURB**

Mot: 3398 lbs-in  
Mresisting: 2781 lbs-in

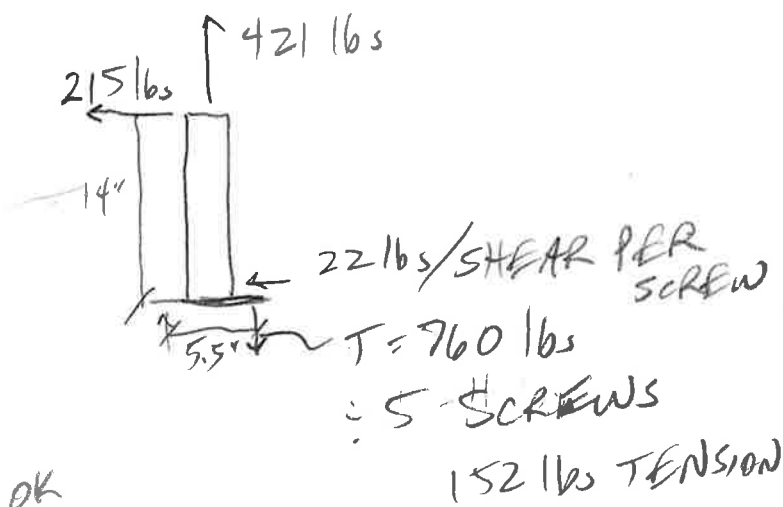
Uplift:	0 lbs (ASD)	Uplift:	13.423309 lbs (ASD)
Shear:	86 lbs (ASD)	Shear:	86 lbs (ASD)

**Check Global Uplift due to wind:**

Uplift Force: 194 lbs

Weight of Unit resisiting: 180 lbs

Net uplift:	14 lbs (ASD)
-------------	--------------



#12 SCREW  
TENSION CAPACITY  
 $T = 154 \text{ lbs} \times 1.6 \times 1''$   
 $= 246 \text{ lbs}$

$V = 116 \text{ lbs} \times 1.6 = 186 \text{ lbs}$

$SR = \frac{22}{186} + \frac{152}{246} = 0.74 \text{ OK}$

EBTN 11.7-1  $\rightarrow z' = 244.5$   
 $SR = 0.63 \text{ OK}$

REFERENCE DETAIL

14" CURB TO TOP OF WOOD FRAMING

#12 SCREWS w/ 2 1/2" LENGTH

$$W = 154 \text{ lbs/in} \times 1.75" = 270 \text{ lbs} = C_o \times C_m$$

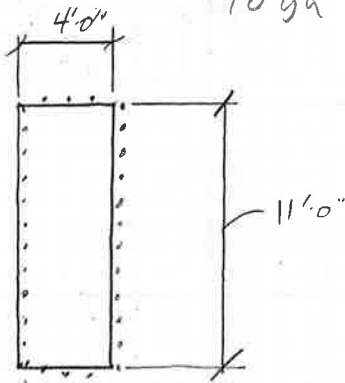
$$= 302 \text{ lbs TENSION}$$

SHEAR CAPACITY

14ga STEEL =  $147 \text{ lbs} \times 1.6 \times 0.7 = 165 \text{ lbs}$

16ga STEEL =  $116 \text{ lbs} \xrightarrow{130}$  ← ASSUME FOR CALCULATION PURP.

18ga STEEL =  $90 \text{ lbs} = 100$



(3) INTERMEDIATE SCREWS  
(12) SCREWS SIDE

30 SCREWS TOTAL IN SHEAR  
12 SCREWS IN TENSION

SHEAR =  $1624 \text{ lbs} / 30 = 56$

TENSION =  $1206 \text{ lbs} / 12 = 100$

~~ASD~~ =  $\frac{100}{56}$   $\phi = 1.75 \text{ lbs}$   
 $\alpha = 60.8^\circ$

$$Z' = \frac{302(130)}{302 \cos^2 59 + 130 \sin^2 59}$$

$$Z' = 230 \text{ lbs}$$

$SR = \frac{115}{225} = 0.50$

OK

SIMPSON SDWS SCREWS ~~W/~~ PENETRATION INFO

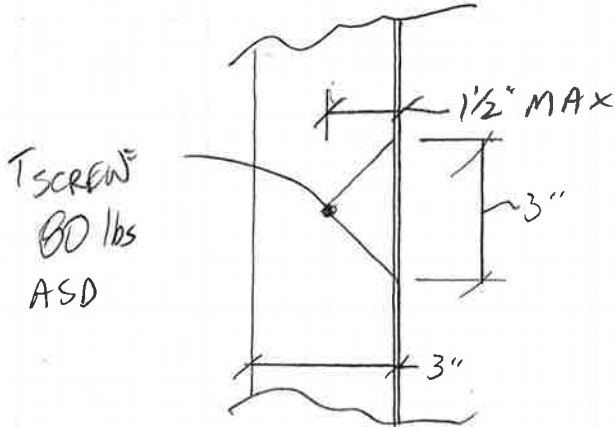
WOOD FRAMING → SHEAR LOADS =  $395 \text{ lbs} \times 1.6 \times 0.7$   
TENSION =  $214 \text{ lbs} \times 1.6 \times 0.7$

SHEAR =  $442 \text{ lbs}$   
TENSION =  $240 \text{ lbs}$  } OK BY INSPECTION

# CHECK CAPACITY OF LIGHT GAGE FLAT PLATE BENDING

ASSUME 16ga 50ksi MATERIAL

1 1/2" DISTANCE FROM C OF SCREW TO BACK WALL OF CURB



T SCREW  
80 lbs  
ASD

$$Z_R = \frac{3(0.0566)^2}{4} = 0.0024 \text{ in}^3$$

$$M_n = Z_R F_y = 50 \text{ ksi} (0.0024 \text{ in}^3)$$

$$M_n = 120 \text{ in-lbs}$$

$$\frac{M_n}{\Omega} = \frac{120 \text{ in-lbs}}{1.67} = 72 \text{ in-lbs}$$

$$\div 1.5" = 48 \text{ lbs}$$

TRY 14 ga MATERIAL

$$Z_R = \frac{3(0.073)^2}{4} = 0.0038 \text{ in}^3$$

$$\frac{M_n}{\Omega} = \frac{50 \text{ ksi} (0.0038 \text{ in}^3)}{1.67}$$

$$\frac{M_n}{\Omega} = 114 \text{ in-lbs} \div 1.5 \text{ in}$$

$$= 76 \text{ lbs}$$

ADD ACTUAL HOLDDOWNS TO CURB

$$\frac{952 \text{ lbs}}{2} = 480 \text{ lbs}$$

USE  
SIMPSON LSTAP  
STRAP w/ (4) #10  
SCREWS TO LIGHT  
GA. CURB &  
(4) 10d NAILS TO  
WOOD CURB

# Gas Fired Packaged Heating & Ventilating Unit Schedule

Line No.	Qty	Unit Tags	Reznor Model-Size	Type	MBH Output	EAT °F	LAT °F	Fuel Type	CFM	Mtr HP	Fan RPM	Ext. SP "WC	Total SP "WC	Voltage & Phase	Unit Notes
1	1	RTU-1	RDH-250	Outdoor					3500	2	901	0.5	0.812	208/3/60	

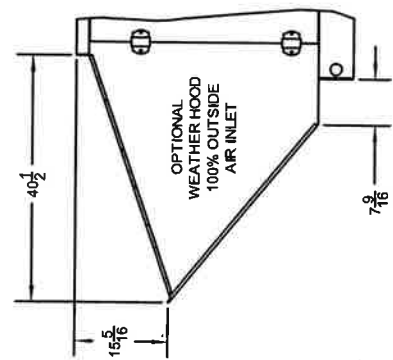
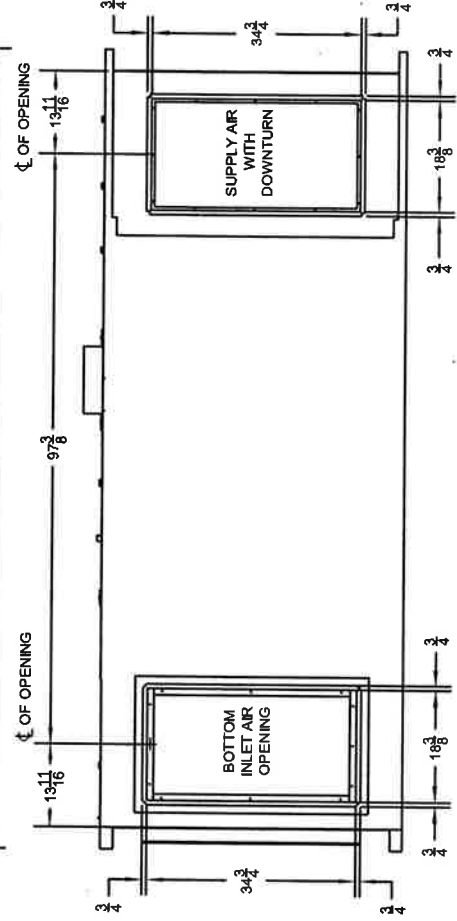
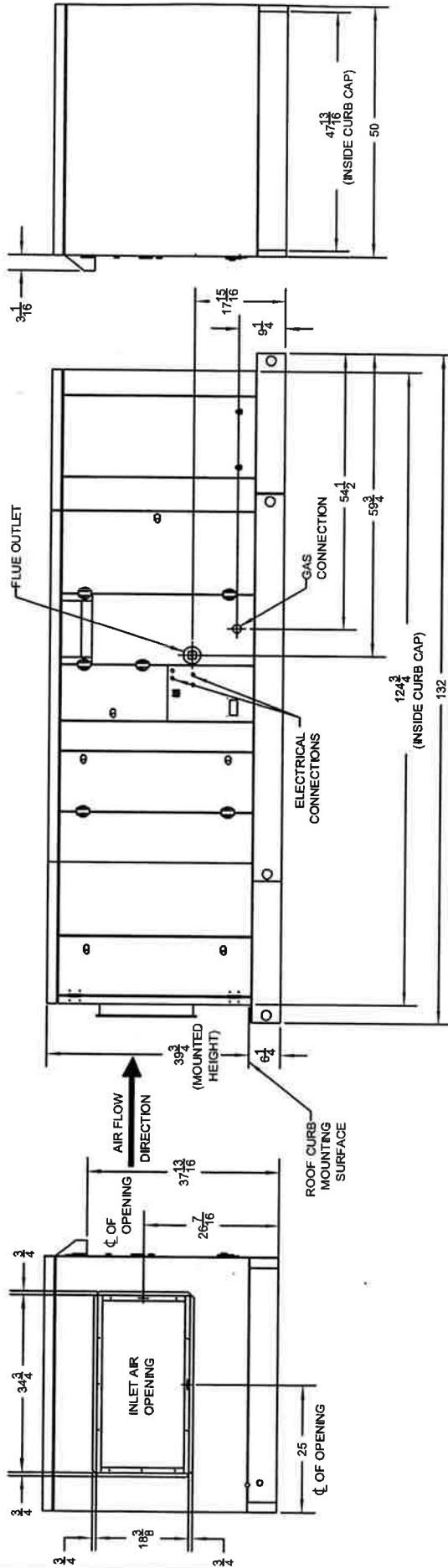
RTU-1  
1700 lb

- Unit Notes:
- 1)
  - 2)
  - 3)
  - 4)
  - 5)

RI

# RDH\_D\_DT\_MX

MODEL(S)  
 - RDH 250  
 - RDH 300



- NOTES:
- 1) UNITS ARE SHOWN WITH LEFT HAND CONTROLS (AJ1).
  - 2) UNITS WITH OPTION AJ2 HAVE GAS AND ELECTRICAL CONNECTIONS/SERVICING ON THE OPPOSITE SIDE.
  - 3) COIL CONNECTIONS ON THE LEFT HAND SIDE (AU5L OR AU6L).
  - 4) UNITS WITH OPTION AU5R OR AU6R HAVE COIL CONNECTIONS ON THE OPPOSITE SIDE.

ALL DIMENSIONS ARE IN INCHES

R2



Applies to All Models unless otherwise noted.

### INLET DAMPERS (Indoor Units)

#### CABINET MOUNTED OPT. ON/OFF DAMPER OPTION AR8

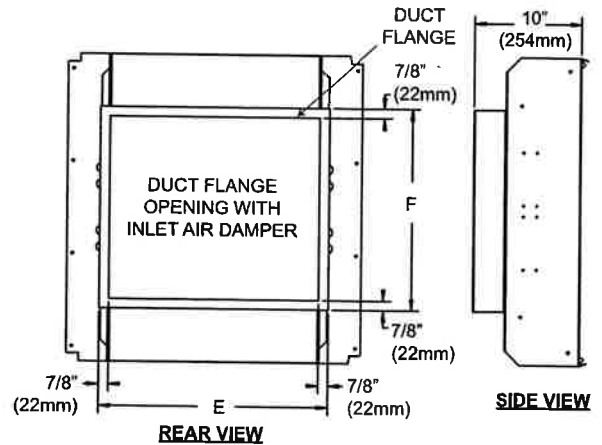
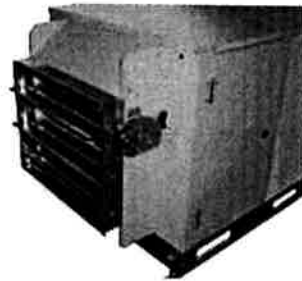
Option AR8 is factory-mounted to the air inlet side of the cabinet. It can be mounted on the blower cabinet or the cooling coil module. See table below for dimensions and weights to be added to base unit. (not available with Evaporative Cooling Module. See Mixing Box Option MXB1 for additional air inlet arrangements.)

##### Dimensions - Inches (±1/8")

PDH or SDH	PEH	PXH	SHH	E	F	Weight - lbs.
75, 100	10A, 20A, 40A	000A	--	19 3/8	16 3/4	34
125, 150	15B, 30B, 60B	000B	--	24 7/8	16 3/4	45
175, 200, 225	--	000C	130, 180	21 1/4	25 3/4	56
250, 300	30D, 60D, 90D, 120D	000D	260	34 1/4	18 1/4	73
350, 400A	40E, 80E, 120E	000E	350	38 5/8	21 1/4	85

##### Dimensions - mm (±3)

PDH or SDH	PEH	PXH	SHH	E	F	Weight - (kg)
75, 100	10A, 20A, 40A	000A	N/A	(492)	(425)	(15)
125, 150	15B, 30B, 60B	000B	N/A	(632)	(425)	(20)
175, 200, 225	--	000C	130, 180	(540)	(654)	(25)
250, 300	30D, 60D, 90D, 120D	000D	260	(870)	(464)	(33)
350, 400A	40E, 80E, 120E	000E	350	(981)	(540)	(39)



### OPTIONAL WEATHER HOOD OPTION AS2

100% Outside Air Screened Intake Hood w/Rain Baffles.

Weather hood shipped separately, knocked down, for field installation.

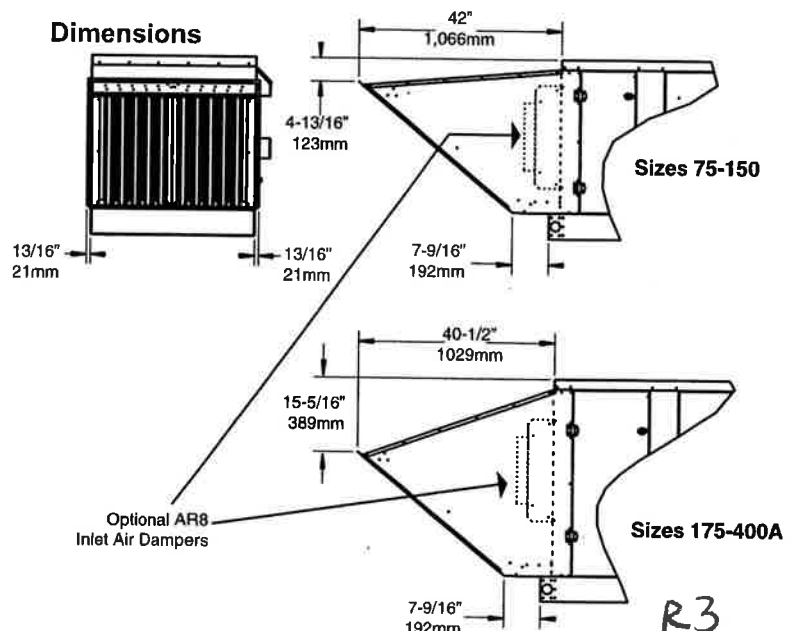
RDH Size	REH Cabinet	RHH Size	RXH Size	lbs	(kg)
75/100	10A, 20A, 40A	--	000A	70	(32)
125/150	15B, 30B, 60B	--	000B	76	(34)
175/200/225	--	130, 180	000C	76	(34)
250/300	30D, 60D, 90D, 120D	260	000D	87	(39)
350/400A	40E, 80E, 120E	350	000E	96	(44)

### INLET DAMPERS (Outdoor Units)

#### CABINET MOUNTED OPT. ON/OFF DAMPER OPTION AR8

Option AR8 is factory-mounted to the air inlet side of the cabinet. It can be mounted on the blower cabinet or the cooling coil module (not available with Evaporative Cooling Module or Mixing Box. See Mixing Box Option MXB1 for additional air inlet arrangements.)

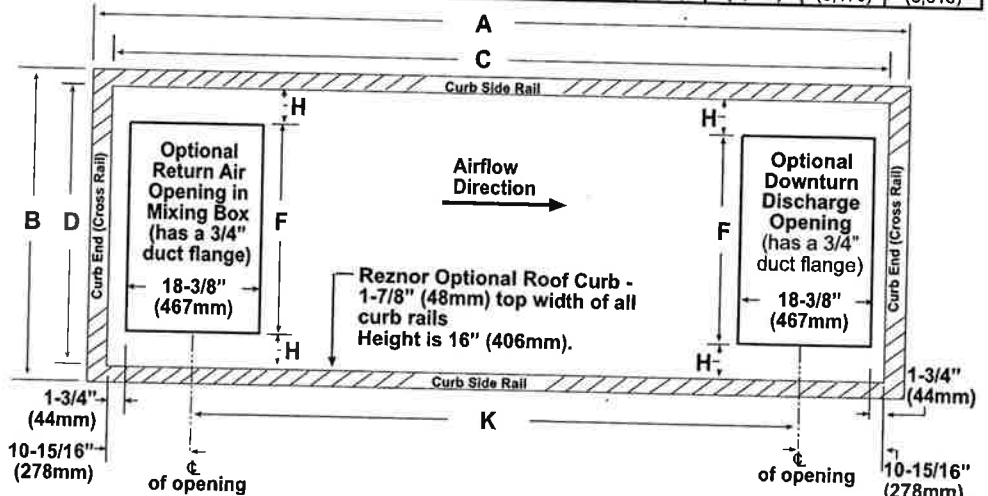
Option AR8 for outdoor models is similar to the inlet damper option for indoor units, except the outdoor units do not included duct flanges.



Curb is 16" (406mm) high

Configuration	Option Code	RDH Size	REH Size	RXH Size	Inches (±1/8)				mm (±3)				Weight	
					A	B	C	D	A	B	C	D	lbs	kg
Basic Unit ONLY (blower and heat section) with horizontal discharge	CJ8A	75/100	10A/20A/40A	000A	51-13/16	29-13/16	48-1/16	26-1/16	1,316	757	1,221	662	90	41
		125/150	15B/30B/60B	000B	51-13/16	39-13/16	48-1/16	36-1/16	1,316	1,011	1,221	916	101	46
		175/200/225	N/A	000C	67-1/2	29-13/16	63-3/4	26-1/16	1,715	757	1,619	662	107	49
		250/300	30D/60D/90D/120D	000D	67-1/2	46-1/16	63-3/4	42-5/16	1,715	1,170	1,619	1,075	125	57
		350/400A	40E/80E/120E	000E	67-1/2	54-1/16	63-3/4	50-5/16	1,715	1,373	1,619	1,278	134	61
Basic unit PLUS 1 either - Downturn Discharge Plenum (AQ5 or AQ8); OR Mixing Box (MXB1) with horizontal discharge; OR Cooling Coil Cabinet without Reheat (AU5 or AU6) with horizontal discharge	CJ8B	75/100	10A/20A/40A	000A	79-9/16	29-13/16	75-13/16	26-1/16	2,021	757	1,926	662	120	54
		125/150	15B/30B/60B	000B	79-9/16	39-13/16	75-13/16	36-1/16	2,021	1,011	1,926	916	131	59
		175/200/225	N/A	000C	95-1/4	29-13/16	91-1/2	26-1/16	2,419	757	2,324	662	138	63
		250/300	30D/60D/90D/120D	000D	95-1/4	46-1/16	91-1/2	42-5/16	2,419	1,170	2,324	1,075	155	70
		350/400A	40E/80E/120E	000E	95-1/4	54-1/16	91-1/2	50-5/16	2,419	1,373	2,324	1,278	164	74
Basic unit PLUS 2 - Down Discharge (AQ 5 or 8) AND Mixing Box OR Cooling Coil Cabinet without Reheat (AU 5 or 6); OR Mixing Box AND Cooling Coil Cabinet without Reheat (AU 5 or 6) with horizontal discharge	CJ8C	75/100	10A/20A/40A	000A	107-5/16	29-13/16	103-9/16	26-1/16	2,726	757	2,631	662	151	68
		125/150	15B/30B/60B	000B	107-5/16	39-13/16	103-9/16	36-1/16	2,726	1,011	2,631	916	162	73
		175/200/225	N/A	000C	123	29-13/16	119-1/4	26-1/16	3,124	757	3,029	662	168	76
		250/300	30D/60D/90D/120D	000D	123	46-1/16	119-1/4	42-5/16	3,124	1,170	3,029	1,075	186	84
		350/400A	40E/80E/120E	000E	123	54-1/16	119-1/4	50-5/16	3,124	1,373	3,029	1,278	195	88
Basic unit PLUS 3 - Down Discharge Plenum (AQ5 or AQ8) AND Mixing Box (MXB1) AND Cooling Coil Cabinet without Reheat (AU5 or AU6)	CJ8D	75/100	10A/20A/40A	000A	135-1/16	29-13/16	131-5/16	26-1/16	3,431	757	3,335	662	181	82
		125/150	15B/30B/60B	000B	135-1/16	39-13/16	131-5/16	36-1/16	3,431	1,011	3,335	916	192	87
		175/200/225	N/A	000C	150-3/4	29-13/16	147	26-1/16	3,829	757	3,734	662	199	90
		250/300	30D/60D/90D/120D	000D	150-3/4	46-1/16	147	42-5/16	3,829	1,170	3,734	1,075	216	98
		350/400A	40E/80E/120E	000E	150-3/4	54-1/16	147	50-5/16	3,829	1,373	3,734	1,278	225	102
Basic unit PLUS 1 - Cooling Coil Cabinet with Reheat (AU7) with horizontal discharge	CJ8E	75/100	10A/20A/40A	000A	104-9/16	29-13/16	100-13/16	26-1/16	2,656	757	2,561	662	149	68
		125/150	15B/30B/60B	000B	104-9/16	39-13/16	100-13/16	36-1/16	2,656	1,011	2,561	916	160	73
		175/200/225	N/A	000C	120-1/4	29-13/16	116-1/2	26-1/16	3,054	757	2,959	662	167	76
		250/300	30D/60D/90D/120D	000D	120-1/4	46-1/16	116-1/2	42-5/16	3,054	1,170	2,959	1,075	184	83
		350/400A	40E/80E/120E	000E	120-1/4	54-1/16	116-1/2	50-5/16	3,054	1,373	2,959	1,278	193	88
Basic unit PLUS 2 - Cooling Coil Cabinet with Reheat (AU7) AND Down Discharge Plenum (AQ5 or AQ8) OR Mixing Box (MXB1) with horizontal discharge	CJ8F	75/100	10A/20A/40A	000A	132-5/16	29-13/16	128-9/16	26-1/16	3,361	757	3,266	662	180	82
		125/150	15B/30B/60B	000B	132-5/16	39-13/16	128-9/16	36-1/16	3,361	1,011	3,266	916	191	87
		175/200/225	N/A	000C	148	29-13/16	144-1/4	26-1/16	3,759	757	3,664	662	197	89
		250/300	30D/60D/90D/120D	000D	148	46-1/16	144-1/4	42-5/16	3,759	1,170	3,664	1,075	215	98
		350/400A	40E/80E/120E	000E	148	54-1/16	144-1/4	50-5/16	3,759	1,373	3,664	1,278	224	102
Basic unit PLUS 3 - Cooling Coil Cabinet with Reheat (AU7) AND Down Discharge Plenum (AQ5 or AQ8) AND Mixing Box (MXB1)	CJ8G	75/100	10A/20A/40A	000A	160-1/16	29-13/16	156-5/16	26-1/16	4,066	757	3,970	662	210	95
		125/150	15B/30B/60B	000B	160-1/16	39-13/16	156-5/16	36-1/16	4,066	1,011	3,970	916	221	100
		175/200/225	N/A	000C	175-3/4	29-13/16	172	26-1/16	4,464	757	4,369	662	228	103
		250/300	30D/60D/90D/120D	000D	175-3/4	46-1/16	172	42-5/16	4,464	1,170	4,369	1,075	245	111
		350/400A	40E/80E/120E	000E	175-3/4	54-1/16	172	50-5/16	4,464	1,373	4,369	1,278	254	115

RDH Size	REH Size	RXH Size	Dimensions (inches ±1/8)						Dimensions (mm ±3)					
			F	H	K (with mixing box and down discharge)			F	H	K (with mixing box and down discharge)				
					(with mixing box and/or down discharge)	no cooling coil module	with a cooling coil module			(with mixing box and/or down discharge)	no cooling coil module	with a cooling coil module		
75/100	10A/20A/40A	000A	22-7/8	1-9/16	81-5/8	109-3/8	134-3/8	(581)	(40)	(2,073)	(2,778)	(3,413)		
125/150	15B/30B/60B	000B	26-1/2	4-3/4	81-5/8	109-3/8	134-3/8	673	(121)	(2,073)	(2,778)	(3,413)		
175/200/225	N/A	000C	22-7/8	1-9/16	97-3/8	125-1/8	150-1/8	(581)	(40)	(2,473)	(3,178)	(3,813)		
250/300	30D/60D/90D/120D	000D	34-3/4	3-3/4	97-3/8	125-1/8	150-1/8	(883)	(96)	(2,473)	(3,178)	(3,813)		
350/400A	40E/80E/120E	000E	45-13/16	2-1/4	97-3/8	125-1/8	150-1/8	(1164)	(57)	(2,473)	(3,178)	(3,813)		



NOTE: If there is an evaporative cooling module, the base of the unit under the evaporative cooling module extends beyond the end of the roof curb. An evaporative cooling module does not affect the length of the roof curb.

R4

OHP=1



# General Data



## Product Specifications

Model No. ①	4TWR5042G1	4TWR5049E1	4TWR5061E1
Electrical Data V/Ph/Hz ②	208/230/1/60	208/230/1/60	208/230/1/60
Min Cir Ampacity	23	28	36
Max Fuse Size (Amps)	40	50	60
Compressors	CLIMATUFF®-SCROLL	CLIMATUFF®-SCROL	CLIMATUFF®-SCROL
RL AMPS - LR AMPS	16.7 - 112	21.8 - 117	26.4 - 134
Outdoor Fan FL Amps	0.74	1.00	2.80
Fan HP	1/8	1/5	1/3
Fan Dia (inches)	26.6	27.6	227.6
Coil	Spine Fin™	Spine Fin™	Spine Fin™
Refrigerant R-410A	9/14-LB/OZ	13/10-LB/OZ	13/12-LB/OZ
Line Size - (in.) O.D. Gas ③	3/4	7/8	1-1/8
Line Size - (in.) O.D. Liquid ③	3/8	3/8	3/8
Dimensions H x W x D (Crated)	42 x 35.1 x 38.7	51 x 35.1 x 38.7	51 x 35.1 x 38.7
Weight - Shpping	277	331	332
Weight - Net	243	294	295
Start Components	NO	NO	YES
Sound Enclosure	YES	NO	NO
Compressor Sump Heat	YES	YES	YES
<b>Optional Accessories: ④</b>			
Anti-short Cycle Timer	TAYASCT501A	TAYASCT501A	TAYASCT501A
Evaporator Defrost Control A/C	AY28X084	AY28X084	AY28X084
Rubber Isolator Kit	BAYISLT101	BAYISLT101	BAYISLT101
Hard Start Kit Scroll	BAYKSKT260	BAYKSKT260	
Extreme Condition Mounting Kit	BAYECMT004	BAYECMT004	BAYECMT004
Snow Leg - Base & Cap 4" High	BAYLEGS002	BAYLEGS002	BAYLEGS002
Snow Leg - 4" Extension	BAYLEGS003	BAYLEGS003	BAYLEGS003
Seacoast Kit	BAYSEAC001	BAYSEAC001	BAYSEAC001
Refrigerant Lineset ⑤	TAYREFLN7*	TAYREFLN3*	TAYREFLN3*

① Certified in accordance with the Air-Source Unitary Heat Pump Equipment certification program which is based on AHRI Standard 210/240.

② Calculated in accordance with N.E.C. Only use HACR circuit breakers or fuses.

③ Standard line lengths - 60'. Standard lift - 60' Suction and Liquid line.

For Greater lengths and lifts refer to refrigerant piping software Pub# 32-3312-01. (\*denotes latest revision)

④ For accessory description and usage, see page 5.

⑤ \* = 15, 20, 25, 30, 40 and 50 foot lineset available.

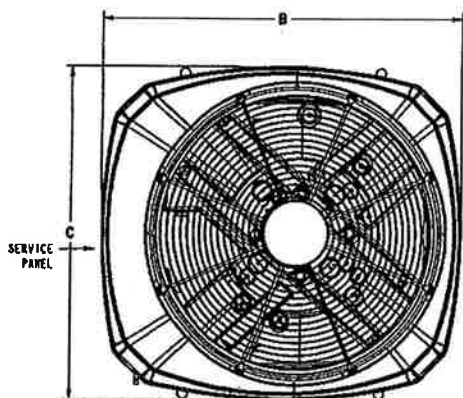
R5

0HP-1



# Dimensions

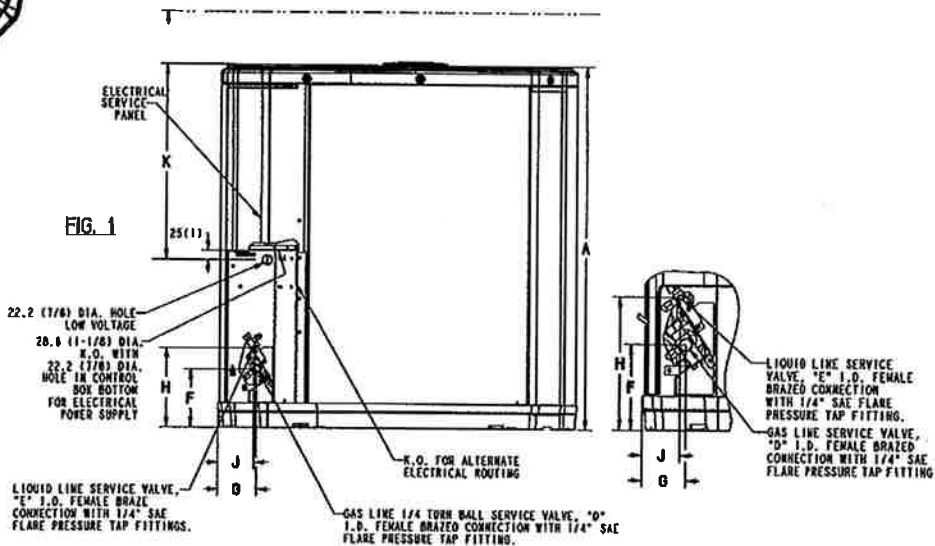
## 4TWR5 Outline Drawing Note: All dimensions are in MM (Inches).



ELECTRICAL AND REFRIGERANT COMPONENT CLEARANCES PER PREVAILING CODES.

TOP DISCHARGE AREA SHOULD BE UNRESTRICTED FOR AT LEAST 1524 (5 FEET) ABOVE UNIT. UNIT SHOULD BE PLACED SO ROOF RUN-OFF WATER DOES NOT POUR DIRECTLY ON UNIT, AND SHOULD BE AT LEAST 305 (12") FROM WALL AND ALL SURROUNDING SURBERENT OR TWO SIDES. OTHER TWO SIDES UNRESTRICTED.

FIG. 1



MODELS	BASE	A	B	C	D	E	F	G	H	J	K
4TWR5018G	4	730 (28-3/4)	829 (32-5/8)	756 (29-3/4)	5/8	3/8	143 (5-5/8)	92 (3-5/8)	210 (8-1/4)	79 (3-1/8)	508 (20)
4TWR5024G	3	832 (32-3/4)	829 (32-5/8)	756 (29-3/4)	5/8	3/8	143 (5-5/8)	92 (3-5/8)	210 (8-1/4)	79 (3-1/8)	508 (20)
4TWR5030G	4	841 (33-1/8)	946 (37-1/4)	870 (34-1/4)	3/4	3/8	152 (6)	98 (3-7/8)	219 (8-5/8)	86 (3-3/8)	508 (20)
4TWR5036G	4	841 (33-1/8)	946 (37-1/4)	870 (34-1/4)	3/4	3/8	152 (6)	98 (3-7/8)	219 (8-5/8)	86 (3-3/8)	508 (20)
4TWR5042G	4	943 (37 1/8)	946 (37-1/4)	870 (34-1/4)	3/4	3/8	143 (5-5/8)	98 (3-7/8)	219 (8-5/8)	86 (3-3/8)	508 (20)
4TWR5049E	4	1147 (45 1/8)	946 (37-1/4)	870 (34-1/4)	7/8	3/8	152 (6)	98 (3-7/8)	219 (8-5/8)	86 (3-3/8)	508 (20)
4TWR5061E	4	1147 (45 1/8)	946 (37-1/4)	870 (34-1/4)	1-1/8	3/8	152 (6)	98 (3-7/8)	219 (8-5/8)	86 (3-3/8)	508 (20)

R6